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| Subject Code | $\begin{gathered} \mathbf{Q} \\ \text { Id } \end{gathered}$ | Questions | Answer Key |
| :---: | :---: | :---: | :---: |
| 606 | 301 | A source $V_{s}(t)=\mathrm{V} \cos 100 \pi t$ has an intemal impedance of $(4+j 3) \Omega$. If a purely resistive load connected to this source has to extract the maximum power out of the source, its value in $\Omega$ should be <br> (A) 3 <br> (B) 4 <br> (C) 5 <br> (D) 7 | (C) |
| 606 | 302 | In the circuit shown below, the value of $R_{L}$ such that the power transferred to $R_{L}$ is maximum is <br> (A) $5 \Omega$ <br> (B) $10 \Omega$ <br> (C) $15 \Omega$ <br> (D) $20 \Omega$ | (C) |
| 606 | 303 | For parallel RLC circuit, which one of the following statements is NOT correct? <br> (A) <br> The bandwidth of the circuit decreases if $R$ is increased <br> (B) The bandwidth of the circuit remains same if $L$ is increased <br> (C) At resonance, input impedance is a real quantity <br> (D) At resonance, the magnitude of input impedance attains its minimum value. | (D) |
| 606 | 304 | In a simple DC circuit with a constant voltage, where the resistance increases current will <br> (A) Decrease <br> (B) Stop <br> (C) Increase <br> (D) Remain constant | (A) |
| 606 | 305 | A fully charged mobile phone with a 12 V battery is good for a 10 minute talk-time. Assume that, during the talk-time the battery delivers a constant current of 2 A and its voltage drops linearly from 12 V to 10 V as shown in the figure. How much energy does the battery deliver during this talk-time? | (C) |


|  |  | (A) 220 J <br> (B) 12 kJ <br> (C) 13.2 kJ <br> (D) 14.4 J |  |
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| 606 | 306 | An independent voltage source in series with an impedance $Z_{s}=R_{s}+j X_{s}$ delivers a maximum average power to a load impedance $Z_{L}$ when <br> (A) $Z_{r}=\mathrm{Rs}+\mathrm{i} \mathrm{Xs}$ <br> (B) $Z_{t}=\mathrm{Rs}$ <br> (C) $Z_{L}=j X_{s}$ <br> (D) $Z_{L}=R_{s}-j X_{s}$ | (D) |
| 606 | 307 | The condition on $R, L$ and $C$ such that the step response $y(t)$ in the figure has no oscillations, is <br> (A) $\mathrm{R} \geq \frac{1}{2} \sqrt{L / C}$ <br> (B) $\mathrm{R} \geq \sqrt{L / C}$ <br> (C) <br> $\mathrm{R} \geq 2 \sqrt{L / C}$ <br> (D) $\mathrm{R}=1 / \sqrt{L / C}$ | (C) |
| 606 | 308 | Voltage follower can be used as a <br> (A) <br> Peak detector <br> (B) <br> Summer <br> (C) <br> Impedance matcher <br> (D) <br> Integrator | (C) |
| 606 | 309 |  | (B) |


|  |  | A square pulse of 3 volts amplitude is applied to $C-R$ circuit shown in the figure. The capacitor is initially uncharged. The output voltage V2 at time $\mathrm{t}=2 \mathrm{sec}$ is <br> (A) <br> 3 V <br> (B) <br> $-3 \mathrm{~V}$ <br> (C) <br> 4 V <br> (D) <br> $-4 \mathrm{~V}$ |  |
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| 606 | 310 | Twelve $1 \Omega$ resistance are used as edges to form a cube. <br> The resistance between two diagonally opposite comers of the cube is <br> (A) $\frac{5}{6} \Omega$ <br> (B) $1 \Omega$ <br> (C) $\frac{6}{5} \Omega$ $\begin{equation*} \frac{3}{2} \Omega \tag{D} \end{equation*}$ | (A) |
| 606 | 311 | The dependent current source shown in the figure <br> (A) delivers 80 W <br> (B) absorbs 80 W <br> (C) delivers 40 W <br> (D) absorbs 40 W | (A) |
| 606 | 312 | A 2-port network is shown in the given figure. The parameter $h_{21}$ for this network can be given by <br> (A) $-1 / 2$ | (A) |


|  |  | (B) $=1 / 2$ <br> (C) $-3 / 2$ <br> (D) $+3 / 2$ |  |
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| 606 | 313 | Superposition theorem is NOT applicable to networks containing <br> (A) nonlinear elements <br> (B) dependent voltage sources <br> (C) dependent current sources <br> (D) transformers | (A) |
| 606 | 314 | A high-Q quartz crystal exhibits series resonance at the frequency $w_{s}$ and parallel resonance at the frequency $w_{p}$. Then <br> (A) $w_{s}$ is very close to, but less than $w_{p}$ <br> (B) $w_{s} \ll w_{p}$ <br> (C) $w_{s}$ is very close to, but greater than $w_{p}$ <br> (D) $w_{s} \gg w_{p}$ | (A) |
| 606 | 315 | The number of independent loops for a network with $n$ nodes and $b$ branches is <br> (A) $n-1$ <br> (B) $b-n$ <br> (C) $b-n+1$ <br> (D) independent of the number of nodes | (C) |
| 606 | 316 | In a forward biased pn junction diode, the sequence of events that best describes the mechanism of current flow is <br> (A) injection, and subsequent diffusion and recombination of minority carriers <br> (B) injection, and subsequent drift and generation of minority carriers <br> (C) extraction, and subsequent diffusion and generation of minority carriers <br> (D) extraction, and subsequent drift and recombination of minority carriers | (A) |
| 606 | 317 | In a MOSFET operating in the saturation region, the channel length modulation effect causes <br> (A) an increase in the gate-source capacitance <br> (B) a decrease in the transconductance <br> (C) a decrease in the unity-gain cutoff frequency <br> (D) a decrease in the output resistance | (D) |
| 606 | 318 | Thin gate oxide in a CMOS process is preferably grown using <br> (A) wet oxidation <br> (B) dry oxidation <br> (C) epitaxial oxidation <br> (D) ion implantation | (B) |
| 606 | 319 | The DC current gain ( $\beta$ ) of a BJT is 50 . Assuming that the emitter injection efficiency is 0.995 , the base transport factor is <br> (A) 0.98 <br> (B) 0.985 | (B) |


|  |  | (C) 0.99 <br> (D) 0.995 |  |
| :---: | :---: | :---: | :---: |
| 606 | 320 | The phenomenon known as "Early Effect" in a bipolar transistor refers to a reduction of the effective base-width caused by <br> (A) Electron - hole recombination at the base <br> (B) The reverse biasing of the base - collector junction <br> (C) The forward biasing of emitter-base junction <br> (D) The early removal of stored base charge during saturation-to-cut off switching | (B) |
| 606 | 321 | A MOS capacitor made using ' p ' type substrate is in the accumulation mode. The dominan charge in the channel is due to the presence of <br> (A) holes <br> (B) electrons <br> (C) positively charged icons <br> (D) negatively charged ions | (B) |
| 606 | 322 | An n-type silicon bar 0.1 cm long and $100 \mu \mathrm{~m}^{2}$ cross-sectional area has a majority carrier concentration of $5 \times 10^{20} / \mathrm{m}^{2}$ and the carrier mobility is $0.13 \mathrm{~m}^{2} / \mathrm{V}$-s at 300 K . If the charge of an electron is $1.5 \times 10^{-19}$ coulomb, then the resistance of the bar is <br> (A) 106 Ohm <br> (B) 104 Ohm <br> (C) 10-1 Ohm <br> (D) 10-4 Ohm | (A) |
| 606 | 323 | A particular green LED emits light of wavelength $5490 \mathrm{~A}^{\circ}$ The energy band gap of the semiconductor material used there is (Plank's constant $=6.626 \times 10^{-34} \mathrm{~J}-\mathrm{s}$ ) <br> (A) 2.26 eV <br> (B) 1.98 eV <br> (C) 1.17 Ev <br> (D) 0.74 eV | (A) |
| 606 | 324 | The static characteristic of an adequately forward biased $p-n$ junction is a straight line, if the plot is of <br> (A) $\log I$ vs $\log V$ <br> (B) $\log I$ vs $V$ <br> (C) $I$ vs $\log V$ <br> (D) $I$ vs $V$ | (B) |
| 606 | 325 | In a bipolar transistor at room temperature, if the emitter current is doubled the voltage across its base-emitter junction <br> (A) doubles <br> (B) halves <br> (C) increases by about 20 mV <br> (D) decreases by about 20 mV | (C) |


| 606 | 326 | The common-emitter short-circuit current gain b of a transistor <br> (A) is a monotonically increasing function of the collector current $I_{C}$ <br> (B) is a monotonically decreasing function of $I_{C}$ <br> (C) 人े and then decreases with further increase in $\mathrm{I}_{\mathrm{C}}$ <br> $(\mathrm{D})$ is not a function of $I_{C}$ | (C) |
| :---: | :---: | :---: | :---: |
| 606 | 327 | For a MOS capacitor fabricated on a $p$-type semiconductor, strong inversion occurs when <br> (A) surface potential is equal to Fermi potential <br> (B) surface potential is zero <br>  potential in magnitude <br> (D) surface potential is positive and equal to twice the Fermi potential | (D) |
| 606 | 328 | An n-channel JEFT has $I_{D S S}=2 \mathrm{~mA}$ and $\mathrm{Vp}=-4 \mathrm{~V}$. Its transconductance $g_{m}$ (in milliohm) for an applied gate-to-source voltage VGS of -2 V is <br> (A) 0.25 <br> (B) 0.5 <br> (C) 0.75 <br> (D) 1.0 | (B) |
| 606 | 329 | If the transistor in the figure is in saturation, then <br> (A) <br> $I_{C}$ is always equal to $\beta_{d c} I_{B}$ <br> (B) <br> $I_{C}$ is always equal to $-\beta_{d c} I_{B}$ <br> (C) <br> $I_{C}$ is greater than or equal to $\beta_{\text {fr }} I_{B}$ <br> (D) <br> $I C$ is less than or equal to $\beta_{d c} I_{\square}$ | (D) |
| 606 | 330 | Choose proper substitutes for X and Y to make the following statement correct Tunnel diode and Avalanche photo diode are operated in X bias ad Y bias respectively. <br> (A) X : reverse, Y : reverse <br> (B) X : reverse, Y : forward <br> (C) X: forward, Y: reverse <br> (D) X: forward, Y: forward | (C) |
| 606 | 331 |  | (D) |


|  |  | The $i-v$ characteristics of the diode in the circuit given below are $\left(\begin{array}{cc}\frac{v-0.7}{500} A & V \geq 07 V \\ 0 A, & V<0.7 V\end{array}\right)$ <br> The current in the circuit is <br> (A) 10 mA <br> (B) 9.3 mA <br> (C) 6.67 mA <br> (D) 6.2 mA |  |
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| 606 | 332 | The circuit below implements a filter between the input current $i_{i}$ and the output voltage $v_{o}$. Assume that the op-amp is ideal. The filter implemented is a <br> (A) low pass filter <br> (B) band pass filter <br> (C) band stop filter <br> (D) high pass filter | (D) |
| 606 | 333 | In the following a stable multivibrator circuit, which properties of $v_{0}(t)$ depend on R2? <br> (A) Only the frequency <br> (B) Only the amplitude <br> (C) Both the amplitude and the frequency <br> (D) Neither the amplitude nor the frequency | (A) |
| 606 | 334 |  | (D) |


|  |  | In the circuit shown below, the op-amp is ideal, the transistor has $V_{B E}=0.6 \mathrm{~V}$ and $\beta=150$. Decide whether the feedback in the circuit is positive or negative and determine the voltage V at the output of the op-amp. <br> (A) Positive feedback, $\mathrm{V}=10 \mathrm{~V}$ <br> (B) Positive feedback, $\mathrm{V}=0 \mathrm{~V}$ <br> (C) Negative feedback, $\mathrm{V}=5 \mathrm{~V}$ <br> (D) Negative feedback, $\mathrm{V}=2 \mathrm{~V}$ |  |
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| 606 | 335 | The OPAMP circuit shown above represents a <br> (A) high pass filter <br> (B) low pass filter <br> (C) band pass filter <br> (D) band reject filter | (B) |
| 606 | 336 | In a transconductance amplifier, it is desirable to have <br> (A) a large input resistance and a large output resistance <br> (B) a large input resistance and a small output resistance <br> (C) aa small input resistance and a large output resistance <br> (D) a small input resistance and a small output resistance | (A) |
| 606 | 337 | For the BJT circuit shown, assume that the $\beta$ of the transistor is very large and $V_{B E}=0.7 \mathrm{~V}$. The mode of operation of the BJT is <br> (A) cut-off <br> (B) saturation <br> (C) normal active <br> (D) reverse active | (B) |
| 606 | 338 |  | (C) |


|  |  | The voltage 00 is indicated in the figure has been measured by an ideal voltmeter. Which of the following can be calculated? <br> (A) Bias current of the inverting input only <br> (B) Bias current of inverting and non-inverting input only <br> (C) Input offset current only <br> (D) Both the bias currents and input offset current |  |
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| 606 | 339 | Both transistors T1 and T2 show in the figure, have a $\beta=100$, threshold voltage of 1 Volts. The device parameters $K_{1}$ and $K_{2}$ of $T_{1}$ and $T_{2}$ are, respectively, $36 \mu \mathrm{~A} / V^{2}$ and $9 \mu \mathrm{~A} V^{2}$. The output voltage Vo is <br> (A) 1 V <br> (B) 2 V <br> (C) 3 V <br> (D) 4 V | (D) |
| 606 | 340 | Voltage series feedback (also called series-shunt feedback) results in <br> (A) increase in both input and output impedances <br> (B) decrease in both input and output impedances <br> (C) increase in input impedance and decrease in output impedance <br> (D) decrease in input impedance and increase in output impedance | (C) |
| 606 | 341 | The circuit shown in the figure is best described as a <br> (A) bridge rectifier <br> (B) ring modulator <br> (C) frequency discriminator <br> (D) voltage doubler | (D) |
| 606 | 342 | If the differential voltage gain and the common mode voltage gain of a differential amplifier are 48 dB and 2 dB | (C) |


|  |  | respectively, then common mode rejection ratio is <br> (A) 23 dB <br> (B) 25 dB <br> (C) 46 dB <br> (D) 50 dB |  |
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| 606 | 343 | Generally, the gain of a transistor amplifier falls at high frequencies due to the <br> (A) internal capacitances of the device <br> (B) coupling capacitor at the input <br> (C) skin effect <br> (D) coupling capacitor at the output | (B) |
| 606 | 344 | Three identical amplifiers with each one having a voltage gain of 50 , input resistance of $1 \mathrm{k} \Omega$ and output resistance of $250 \Omega$ are cascaded. The opened circuit voltages gain of the combined amplifier is <br> (A) 49 dB <br> (B) 51 dB <br> (C) 98 dB <br> (D) 102 dB | (C) |
| 606 | 345 | Assume that the op-amp of the figure is ideal. If $v_{i}$ is a triangular wave, then $v_{0}$ will be <br> (A) square wave <br> (B) triangular wave <br> (C) parabolic wave <br> (D) sine wave | (A) |
| 606 | 346 | If the op-amp in the figure has an input offset voltage of 5 mV and an open-loop voltage gain of 10000 , then $v_{0}$ will be <br> (A) 0 V <br> (B) 5 mV <br> (C) +15 V or -15 V <br> (D) +50 V or -50 V | (C) |
| 606 | 347 | A dc power supply has a no-load voltage of 30 V , and a full-load voltage of 25 V at a full-load current of 1 A . Its output resistance and load regulation, respectively, are <br> (A) $5 \Omega$ and $20 \%$ | (B) |


|  |  | (B) $25 \Omega$ and $20 \%$ <br> (C) $5 \Omega$ and $16.7 \%$ <br> (D) $25 \Omega$ and $16.7 \%$ |  |
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| 606 | 348 | For full wave rectification, a four diode bridge rectifier is claimed to have the following advantages over a two diode circuit (1) less expensive transformer, (2) smaller size transformer, and (3) suitability for higher voltage application. Of these, <br> (A) only (1) and (2) are true <br> (B) only (1) and (3) are true <br> (C) only (2) and (3) are true <br> (D) (1), (2) as well as (3) are true | (D) |
| 606 | 349 | A zener diode in the circuit shown in the figure has a knee current of 5 mA , and a maximum allowed power dissipation of 300 mW . What are the minimum and maximum load currents that can be drawn safely from the circuit, keeping the output voltage $V_{0}$ constant at 6 V ? <br> (A) $0 \mathrm{~mA}, 180 \mathrm{~mA}$ <br> (B) $5 \mathrm{~mA}, 110 \mathrm{~mA}$ <br> (C) $10 \mathrm{~mA}, 55 \mathrm{~mA}$ <br> (D) $60 \mathrm{~mA}, 180 \mathrm{~mA}$ | (C) |
| 606 | 350 | For small signal ac operation, a practical forward biased diode can be modelled as <br> (A) a resistance and a capacitance in series <br> (B) an ideal diode and resistance in parallel <br> (C) a resistance and an ideal diode in series <br> (D) a resistance | (C) |
| 606 | 351 | The output $Y$ of a 2-bit comparator is logic 1 whenever the 2 -bit input $A$ is greater than the 2-bit input $B$. The number of combinations for which the output is logic 1 , is <br> (A) 4 <br> (B) 6 <br> (C) 8 <br> (D) 10 | (B) |
| 606 | 352 | The full form of the abbreviations TTL and CMOS in reference to logic families are <br> (A) Triple Transistor Logic and Chip Metal Oxide Semiconductor <br> (B) Tristate Transistor Logic and Chip Metal Oxide Semiconductor <br> (C) Transistor Transistor Logic and Complementary Metal Oxide Semiconductor <br> (D) Tristate Transistor Logic and Complementary Metal Oxide Silicon | (C) |
| 606 | 353 | What are the minimum number of 2- to -1 multiplexers required to generate a 2-input AND Gate and a 2-input Ex-OR gate <br> (A) 1 and 2 | (A) |


|  |  | (B) 1 and 3 <br> (C) 1 and 1 <br> (D) 2 and 2 |  |
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| 606 | 354 | $X=01110$ and $Y=11001$ are two 5-bit binary numbers represented in two's complement format. The sum of $X$ and Y represented in two's complement format using 6 bits is <br> (A) 100111 <br> (B) 10000 <br> (C) 101001 <br> (D) correction in key | (C) |
| 606 | 355 | Decimal 43 in Hexadecimal and BCD number system is respectively <br> (A) B2, 0100011 <br> (B) 2B, 01000011 <br> (C) 2B, 00110100 <br> (D) B2, 01000100 | (B) |
| 606 | 356 | A digital system is required to amplify a binary-encoded audio signal. The user should be able to control the gain of the amplifier from minimum to a maximum in 100 increments. The minimum number of bits required to encode, in straight binary, is <br> (A) 8 <br> (B) 6 <br> (C) 5 <br> (D) 7 | (D) |
| 606 | 357 | The minimum number of comparators required to build an 8-bits flash ADC is <br> (A) 8 <br> (B) 63 <br> (C) 255 <br> (D) 256 | (C) |
| 606 | 358 | A 4 bit ripple counter and a bit synchronous counter are made using flip flops having a propagation delay of 10 ns each. If the worst case delay in the ripple counter and the synchronous counter be R and S respectively, then <br> (A) $\mathrm{R}=10 \mathrm{~ns}, \mathrm{~S}=40 \mathrm{~ns}$ <br> (B) $\mathrm{R}=40 \mathrm{~ns}, \mathrm{~S}=10 \mathrm{~ns}$ <br> (C) $\mathrm{R}=10 \mathrm{~ns}, \mathrm{~S}=30 \mathrm{~ns}$ <br> (D) $\mathrm{R}=30 \mathrm{~ns}, \mathrm{~S}=10 \mathrm{~ns}$ | (B) |
| 606 | 359 | 4 - bit 2 's complement representation of a decimal number is 1000 . The number is $(\mathrm{A})+8$ <br> (B) 0 <br> (C) -7 <br> (D) -8 | (D) |
| 606 | 360 | An 8 bit successive approximation analog to digital communication has full scale reading of 2.55 V and its conversion time for an analog input of 1 V is 20 s. The conversion time for a 2 V input will be <br> (A) 10 | (B) |


|  |  | (B) 20 <br> (C) 40 <br> (D) 50 |  |
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| 606 | 361 | The resolution of a 4-bit counting ADC is 0.5 volts. For an analog input of 6.6 volts, the digital output of the ADC will be <br> (A) 1011 <br> (B) 1101 <br> (C) 1100 <br> (D) 1110 | (B) |
| 606 | 362 | Two 2's complement number having sign bits ' $x$ ' and ' $y$ ' are added and the sign bit of the result is $z$. Then, the occurrence of overflow is indicated by the Boolean function <br> (A) <br> xyz <br> (B) <br> $\overline{x y z}$ <br> (C) $\overline{x y} z+x y \bar{z}$ <br> (D) $x y+y z+z x$ | (D) |
| 606 | 363 | The advantage of using a dual slope ADC in a digital voltmeter is that <br> (A) its conversion time is small <br> (B) its accuracy is high <br> (C) it gives output in BCD format <br> (D) it does not require a | (B) |
| 606 | 364 | A dynamic RAM cell which hold 5 V has to be refreshed every 20 m sec , so that the stored voltage does not fall by more than 0.5 V . If the cell has a constant discharge current of 1 pA , the storage capacitance of the cell is <br> (A) $4 \times 10^{-6} \mathrm{~F}$ <br> (B) $4 \times 10^{-9} \mathrm{~F}$ <br> (C) $4 \times 10^{-12} \mathrm{~F}$ <br> (D) $4 \times 10^{-15} \mathrm{~F}$ | (D) |
| 606 | 365 | A memory system of size 26 K bytes is required to be designed using memory chips which have 12 address lines and 4 data lines each. The number of such chips required to design the memory system is <br> (A) 2 <br> (B) 4 <br> (C) 8 <br> (D) 13 | (D) |
| 606 | 366 | A band-limited signal with a maximum frequency of 5 kHz is to be sampled. According to the sampling theorem, the sampling frequency which is not valid is <br> (A) 5 kHz <br> (B) 12 kHz | (A) |


|  |  | (C) 15 kHz <br> (D) 20 kHz |  |
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| 606 | 367 | The input $x(t)$ and output $y(t)$ of a system are related as $y(t)=\int_{-\infty}^{t} x(\tau) \cos (3 \cos (3 \tau) \mathrm{d} \tau$. The system is <br> (A) time-invariant and stable <br> (B) stable and not time-invariant <br> (C) time-invariant and not stable <br> (D) not time-invariant and not stable | (D) |
| 606 | 368 | A system is defined by its impulse response $h(n)=2^{n} u(n-2)$. The system is <br> (A) stable and causal <br> (B) causal but not stable <br> (C) stable but not causal <br> (D) unstable and non-causal | (B) |
| 606 | 369 | The unit impulse response of a system is $f(t)=e^{-t}, t \geq 0$. <br> For this system the steady-state value of the output for unit step input is equal to <br> (A) -1 <br> (B) 0 <br> (C) 1 <br> (D) $\infty$ | (C) |
| 606 | 370 | The power in the signal $s(t)=8 \cos \left(20 \pi-\frac{\pi}{2}\right)+4 \sin (15 \pi t)$ is <br> (A) 40 <br> (B) 41 <br> (C) 42 <br> (D) 82 | (A) |
| 606 | 371 | The Fourier transform of a conjugate symmetric function is always <br> (A) imaginary <br> (B) conjugate anti-symmetric <br> (C) real <br> (D) conjugate symmetric | (C) |
| 606 | 372 | The Laplace transform of $i(t)$ is given by $i(s)=\frac{2}{s(s+1)}$ At $t \rightarrow \infty$ the value of $i(t)$ becomes <br> (A) 0 <br> (B) 1 <br> (C) 2 | (C) |


|  |  | (D) 3 |  |
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| 606 | 373 | Convolution of $x(t+5)$ with impulse function $\partial(t-7)$ is equal to <br> (A) $x(t-12)$ <br> (B) $x(t+12)$ <br> (C) $x(t-2)$ <br> (D) $x(t+2)$ | (C) |
| 606 | 374 | If a signal $f(t)$ has energy E , the energy of the signal $f(2 t)$ is equal to <br> (A) 1 <br> (B) $\mathrm{E} / 2$ <br> (C) 2 E <br> (D) 4 E | (B) |
| 606 | 375 | A signal $x(t)$ has a Fourier transform $\mathrm{X}(\propto)$. If $x(t)$ is a real and odd function of $t$, then $\mathrm{X}(\Phi)$ is <br> (A) a real and even function of $\omega$ <br> (B) a imaginary and odd function of $\omega$ <br> (C) an imaginary and even function of $\omega$ <br> (D) a real and odd function of $\omega$ | (A) |
| 606 | 376 | The return loss of a device is found to be 20 dB . The voltage standing wave ratio (VSWR) and magnitude of reflection coefficient are respectively <br> (A) 1.22 and 0.1 <br> (B) 0.81 and 0.1 <br> (C) - 1.22 and 0.1 <br> (D) 2.44 and 0.2 | (A) |
| 606 | 377 | A plane wave propagating in air with $E\left(8 a_{x}+6 a_{y}+5 a_{z}\right) e^{j(\omega t+3 x-4 y)} \mathrm{V} / \mathrm{m}$ is incident on a perfectly conducting slab positioned at $x \leq 0$. The $E$ field of the reflected wave is <br> (A) $\left(-8 a_{x}-6 a_{y}-5 a_{z}\right) e^{j(\omega t+3 x+4 y)} \mathrm{V} / \mathrm{m}$ <br> (B) $\left(-8 a_{x}+6 a_{y}-5 a_{z}\right) e^{j(\omega t+3 x+4 y) \cdot \mathrm{V} / \mathrm{m}}$ <br> (C) $\left(-8 a_{x}-6 a_{y}-5 a_{z}\right) e^{j(\omega t-3 x-4 y)} \mathrm{V} / \mathrm{m}$ <br> (D) $\left(-8 a_{x}+6 a_{y}-5 a_{z}\right) e^{j(\omega t-3 x-4 y)} \mathrm{V} / \mathrm{m}$ | (C) |
| 606 | 378 |  | (A) |


|  |  | The radiation pattern of an antenna in spherical co-ordinates is given by $F(\theta)=\cos ^{4} \theta ; \quad 0 \leq \theta \leq \pi / 2$. The directivity of the antenna is <br> (A) 10 dB <br> (B) 12.6 dB <br> (C) 11.5 dB <br> (D) 18 dB |  |
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| 606 | 379 | A transmission line with a characteristic impedance of $100 \Omega$ is used to match a $50 \Omega$ section to a $200 \Omega$ section. If the matching is to be done both at 429 MHz and 1 GHz , the length of the transmission line can be approximately <br> (A) 82.5 cm <br> (B) 1.05 m <br> (C) 1.58 cm <br> (D) 1.75 m | (C) |
| 606 | 380 | A transmission line of characteristic impedance $50 \Omega$ is terminated by a $50 \Omega$ load. When excited by a sinusoidal voltage source at 10 GHz , the phase difference between two points spaced 2 mm apart on the line is found to be $\pi / 4$ radians. The phase velocity of the wave along the line is <br> (A) $0.8 \geqslant 10^{8} \mathrm{~m} / \mathrm{s}$ <br> (B) $1.2 \curvearrowright 10^{8} \mathrm{~m} / \mathrm{s}$ <br> (C) $1.6>10^{8} \mathrm{~m} / \mathrm{s}$ <br> (D) $3<10^{8} \mathrm{~m} / \mathrm{s}$ | (C) |
| 606 | 381 | A transmission line has a characteristic impedance of $50 \Omega$ and a resistance of $0.1 \Omega / \mathrm{m}$. If the line is distortion less, the attenuation constant (in $\mathrm{Np} / \mathrm{m}$ ) is <br> (A) 500 <br> (B) 5 <br> (C) 0.014 <br> (D) 0.002 | (D) |
| 606 | 382 | The electric field component of a time harmonic plane EM wave traveling in a nonmagnetic lossless dielectric medium has an amplitude of $1 \mathrm{~V} / \mathrm{m}$. If the relative permittivity of the medium is 4 , the magnitude of the timeaverage power density vector (in $\mathrm{W} / \mathrm{m} 2$ ) is <br> (A) <br> $\frac{1}{30 \pi}$ <br> (B) $\frac{1}{60 \pi}$ <br> (C) $\frac{1}{120 \pi}$ <br> (D) $\frac{1}{240 \pi}$ | (C) |
| 606 | 383 | For a Hertz dipole antenna, the half power beam width (HPBW) in the $E$-plane is <br> (A) $360^{\circ}$ <br> (B) $180^{\circ}$ | (C) |


|  |  | (C) $90^{\circ}$ <br> (D) $45^{\circ}$ |  |
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| 606 | 384 | A uniform plane wave in the free space is normally incident on an infinitely thick dielectric slab (dielectric constant $\varepsilon=9$ ). The magnitude of the reflection coefficient is <br> (A) 0 <br> (B) 0.3 <br> (C) 0.5 <br> (D) 0.8 | (C) |
| 606 | 385 | In the design of a single mode step index optical fibre close to upper cut-off, the single-mode operation is not preserved if <br> (A) radius as well as operating wavelength are halved <br> (B) radius as well as operating wavelength are doubled <br> (C) radius is halved and operating wavelength is doubled <br> (D) radius is doubled and operating wavelength is halved | (B) |
| 606 | 386 | The electric field of an electromagnetic wave propagation in the positive direction is given by $E=\hat{a}_{x} \sin (\omega t-\beta z)+\hat{a}_{y} \sin (\omega t-\beta z+\pi / 2)$. The wave is <br> (A) Linearly polarized in the $z$-direction <br> (B) Elliptically polarized <br> (C) Left-hand circularly polarized <br> (D) Right-hand circularly polarized | (C) |
| 606 | 387 | A transmission line is feeding 1 watt of power to a horn antenna having a gain of 10 dB . The antenna is matched to the transmission line. The total power radiated by the horn antenna into the free space is <br> (A) 10 Watts <br> (B) 1 Watts <br> (C) 0.1 Watts <br> (D) 0.01 Watt | (A) |
| 606 | 388 | A rectangular wave guide having $T E_{10}$ mode as dominant mode is having a cut off frequency 18 GHz for the mode $T E_{30}$. The inner broad-wall dimension of the rectangular wave guide is <br> (A) $5 / 3 \mathrm{~cm}$ <br> (B) 5 cm <br> (C) $5 / 2 \mathrm{~cm}$ <br> (D) 10 cm | (C) |
| 606 | 389 | Refractive index of glass is 1.5 . Find the wavelength of a beam of light with frequency of 1014 Hz in glass. Assume velocity of light is $3 \geqslant 108 \mathrm{~m} / \mathrm{s}$ in vacuum <br> (A) $3>\mathrm{m}$ <br> (B) 3 mm <br> (C) 2 m <br> (D) 1 mm | (C) |
| 606 | 390 | Consider a lossless antenna with a directive gain of +6 dB . If 1 mW of power is fed to it the total power radiated | (A) |


|  |  | by the antenna will be <br> (A) 4 mW <br> (B) 1 mW <br> (C) 7 mW <br> (D) $1 / 4 \mathrm{~mW}$ |  |
| :---: | :---: | :---: | :---: |
| 606 | 391 | A plane electromagnetic wave propagating in freespace is incident normally on a large slab of loss-less, nonmagnetic, dielectric material with $\varepsilon>\mathcal{E}$. Maxima and minima are observed when the electric field is measured in front of the slab. The maximum electric field is found to be 5 times the minimum field. The intrinsic impedance of the medium should be <br> (A) $120 \pi \Omega$ <br> (B) $60 \pi \Omega$ <br> (C) $600 \pi \Omega$ <br> (D) $24 \pi \Omega$ | (D) |
| 606 | 392 | The depth of penetration of electromagnetic wave in a medium having conductivity ' $\sigma$ ' at a frequency of 1 MHz is 25 cm . The depth of penetration at a frequency of 4 MHz will be <br> (A) 6.25 dm <br> (B) 12.50 cm <br> (C) 50.00 cm <br> (D) 100.00 cm | (B) |
| 606 | 393 | A uniform plane wave traveling in air is incident on the plane boundary between air and another dielectric medium with $\varepsilon_{r}=4$. The reflection coefficient for the normal incidence, is <br> (A) Zero <br> (B) $0.5 \angle 180.0$ <br> (C) $0.333 \angle 0.0$ <br> (D) $0.333 \angle 180.0$ | (D) |
| 606 | 394 | The VSWR can have any value between <br> (A) 0 and 1 <br> (B) -1 and +1 <br> (C) 0 and $\infty$ <br> (D) 1 and $\infty$ | (D) |
| 606 | 395 | A person with receiver is 5 Km away from the transmitter. What is the distance that this person must move further to detect a $3-\mathrm{dB}$ decrease in signal strength? <br> (A) 942 m <br> (B) 2070 m <br> (C) 4978 m <br> (D) 5320 m | (B) |
| 606 | 396 | A material has conductivity of $10^{-2} \mathrm{mho} / \mathrm{m}$ and a relative permittivity of 4 . The frequency at which the conduction current in the medium is equal to the displacement current is <br> (A) 45 MHz <br> (B) 90 MHz | (A) |


|  |  | (C) 450 MHz <br> (D) 900 MHz |  |
| :---: | :---: | :---: | :---: |
| 606 | 397 | A uniform plane electromagnetic wave incident on a plane surface of a dielectric material is reflected with a VSWR of 3. What is the percentage of incident power that is reflected? <br> (A) 0.1 <br> (B) 0.25 <br> (C) 0.5 <br> (D) 0.75 | (B) |
| 606 | 398 | The depth of penetration of wave in a lossy dielectric increases with increasing <br> (A) conductivity <br> (B) permeability <br> (C) wavelength <br> (D) permittivity | (C) |
| 606 | 399 | Some unknown material has a conductivity of $10^{6} \mathrm{mho} / \mathrm{m}$ and a permeability of $4 \pi \times 10^{-7} \mathrm{H} / \mathrm{m}$. The skin depth for the material at 1 GHz is <br> (A) $15.9 \geqslant \mathrm{~m}$ <br> (B) $20.9 \geqslant \mathrm{~m}$ <br> (C) $25.9 \geqslant \mathrm{~m}$ <br> (D) $30.9 \geqslant \mathrm{~m}$ | (A) |
| 606 | 400 | A lossless transmission line having $50 \Omega$ characteristic impedance and length $\lambda / 4$ is short circuited at one end and connected to an ideal voltage source of 1 V at the other end. The current drawn from the voltage source is <br> (A) 0 <br> (B) 0.02 A <br> (C) $\infty$ <br> (D) None of the above | (A) |
| 606 | 401 | If $R(\zeta)$ is the auto correlation function of a real, wide-sense stationary random process, then which of the following is NOT true <br> (A) $R(\zeta)=R(-\zeta)$ <br> (B) $R(\zeta) \leq R(0)$ <br> (C) $R(\zeta)=-R(-\zeta)$ <br> (D) <br> The mean square value of the process is $R(0)$ | (C) |
| 606 | 402 |  | (B) |


|  |  | If $S(f)$ is the power spectral density of a real, wide-sense stationary random process, then which of the following is ALWAYS true? <br> (A) $S(0) \leq S(f)$ <br> (B) $S(f) \geq 0$ <br> (C) $S(-f)=-S(f)$ <br> (D) $\int_{-\infty}^{\infty} S(f) d f=0$ |  |
| :---: | :---: | :---: | :---: |
| 606 | 403 | If $E$ denotes expectation, the variance of a random variable $X$ is given by <br> (A) $E\left[X^{2}\right]-E^{2}[X]$ <br> (B) $E\left[X^{2}\right]+E^{2}[X]$ <br> (C) $E\left[X^{2}\right]$ <br> (D) $E^{2}[X]$ | (A) |
| 606 | 404 | A zero-mean white Gaussian noise is passes through an ideal low pass filter of bandwidth 10 kHz . The output is then uniformly sampled with sampling period $t s=0.03 \mathrm{msec}$. The samples so obtained would be <br> (A) correlated <br> (B) statistically independent <br> (C) uncorrelated <br> (D) orthogonal | (A) |
| 606 | 405 | A 1 mW video signal having a bandwidth of 100 MHz is transmitted to a receiver through cable that has 40 dB loss. If the effective one-side noise spectral density at the receiver is $10^{-20} \mathrm{Watt} / \mathrm{Hz}$, then the signal-to-noise ratio at the receiver is <br> (A) 50 dB <br> (B) 30 dB <br> (C) 40 dB <br> (D) 60 dB | (A) |
| 606 | 406 | Two sinusoidal signals of same amplitude and frequencies 10 kHz and 10.1 kHz are added together. The combined signal is given to an ideal frequency detector. The output of the detector is <br> (A) 0.1 kHz sinusoid <br> (B) 20.1 kHz sinusoid <br> (C) a linear function of time <br> (D) a constant | (A) |
| 606 | 407 | The noise at the input to an ideal frequency detector is white. The detector is operating above threshold. The power spectral density of the noise at the output is <br> (A) raised-cosine <br> (B) flat <br> (C) parabolic <br> (D) Gaussian | (C) |


| 606 | 408 | Let $X$ and $Y$ be two statistically independent random variables uniformly distributed in the ranges $(-1,1)$ and $(-2,1)$ respectively. Let $Z=X+Y$. Then the probability that $(z \leq-1)$ is <br> (A) <br> zero <br> (B) <br> $\frac{1}{6}$ <br> (C) <br> $\frac{1}{3}$ <br> (D) <br> $\frac{1}{12}$ | (D) |
| :---: | :---: | :---: | :---: |
| 606 | 409 | Let $Y$ and $Z$ be the random variable obtained by sampling $X(t)$ at $t=2$ and $t=4$ respectively. Let $W=Y-Z$. The variance of $W$ is <br> (A) 13.36 <br> (B) 9.36 <br> (C) 2.64 <br> (D) 8 | (C) |
| 606 | 410 | The line-of-sight communication requires the transmit and receive antennas to face each other. If the transmit antenna is vertically polarized, for best reception the receiver antenna should be <br> (A) horizontally polarized <br> (B) vertically polarized <br> (C) at $45^{\circ}$ with respect to horizontal polarization <br> (D) at $45^{\circ}$ with respect to vertical polarization | (B) |
| 606 | 411 | A band-limited signal with a maximum frequency of 5 kHz is to be sampled. According to the sampling theorem, the sampling frequency, which is not valid, is <br> (A) 5 kHz <br> (B) 12 kHz <br> (C) 15 kHz <br> (D) 20 kHz | (A) |
| 606 | 412 | The PDF of a Gaussian random variable X is given by $p_{x}(\mathrm{X})=\frac{1}{3 \sqrt{2 \pi}} e^{\frac{(x-4)^{2}}{18}}$. The probability of the event $\{X=4\}$ is <br> (A) <br> $\frac{1}{2}$ <br> (B) <br> $\frac{1}{3 \sqrt{2 \pi}}$ <br> (C) | (A) |


|  |  | $0$ <br> (D) $\frac{1}{4}$ |  |
| :---: | :---: | :---: | :---: |
| 606 | 413 | The amplitude spectrum of a Gaussian pulse is <br> (A) uniform <br> (B) a sine function <br> (C) Gaussian <br> (D) an impulse function | (C) |
| 606 | 414 | The Fourier transform of a voltage signal $x(t)$ is $X(f)$. The unit of $X(f)$ is <br> (A) volt <br> (B) volt-sec <br> (C) volt/sec <br> (D) $\operatorname{vol} t^{2}$ | (A) |
| 606 | 415 | The auto correlation function of an energy signal has <br> (A) no symmetry <br> (B) conjugate symmetry <br> (C) odd symmetry <br> (D) even symmetry | (D) |
| 606 | 416 | If $x=\sqrt{-1}$, then the value of $x^{x}$ is <br> (A) $e^{-\pi / 2}$ <br> (B) $e^{\pi / 2}$ <br> (C) $x$ <br> (D) <br> 1 | (A) |
| 606 | 417 | A fair dice is tossed two times. The probability that the second toss results in a value that is higher than the first toss is <br> (A) $2 / 36$ <br> (B) $2 / 6$ <br> (C) $5 / 12$ <br> (D) | (D) |
| 606 | 418 | The order of the differential equation $\frac{d^{2 y}}{d t}+\left(\frac{d y}{d t}\right)^{3}+y^{4}=e^{-t}$ is <br> (A) 1 <br> (B) 2 | (B) |


|  |  | (C) 3 <br> (D) 4 |  |
| :---: | :---: | :---: | :---: |
| 606 | 419 | The system of linear equations $\begin{aligned} & 4 x+2 y=7 \\ & 2 x+y=6 \\ & \text { Has } \end{aligned}$ <br> (A) a unique solution <br> (B) no solution <br> (C) an infinite number of solutions <br> (D) exactly two distinct solutions | (B) |
| 606 | 420 | A probability density function is of the form $\mathrm{p}(\mathrm{x})=\mathrm{K} e^{-\alpha(x)} \mathrm{x} \in(-\infty, \infty)$. The value of $K$ is <br> (A) 0.5 <br> (B) 1 <br> (C) 0.5 a <br> (D) a | (C) |
| 606 | 421 | Three Capacitors $\mathrm{C}_{1}, \mathrm{C}_{2}$ and $\mathrm{C}_{3}$ whose values are $10 \mu \mathrm{~F}, 5 \mu \mathrm{~F}, 2 \mu \mathrm{~F}$ respectively have breakdown $10 \mathrm{~V}, 5 \mathrm{~V}$ and 2 V respectively. For the interconnection shown below the maximum safe voltage in Volts that can be applied across the combination, and the corresponding total charge in $\mu \mathrm{C}$ stored in the effective capacitance across the terminals are respectively <br> (A) 2.8 and 36 <br> (B) 7 and 119 <br> (C) 2.8 and 32 <br> (D) 7 and 80 | (C) |
| 606 | 422 | The average power delivered to an impedance (4-j3) $\Omega$ by a current $5 \cos (100 \mathrm{pt}+100) \mathrm{A}$ is <br> (A) 44.2 W <br> (B) 50 W <br> (C) 62.5 W <br> (D) 125 W | (B) |
| 606 | 423 | In a series $R L C$ circuit, $R=2 \mathrm{k} \Omega, L=1 \mathrm{H}$, and $C=1 / 400 \mu \mathrm{~F}$. The resonant frequency is <br> (A) $2 \times 10^{4} \mathrm{~Hz}$ <br> (B) $1 / \pi \times 10^{4} \mathrm{~Hz}$ | (B) |


|  |  | (C) $10^{4} \mathrm{~Hz}$ <br> (D) $2 \pi \times 10^{4} \mathrm{~Hz}$ |  |
| :---: | :---: | :---: | :---: |
| 606 | 424 | The first and the last critical frequency of an $R C$-driving point impedance function must respectively be <br> (A) a zero and a pole <br> (B) a zero and a zero <br> (C) a pole and a pole <br> (D) a pole and a zero | (C) |
| 606 | 425 | A source of angular frequency $1 \mathrm{rad} / \mathrm{sec}$ has a source impedance consisting of $1 \Omega$ resistance in series with 1 H inductance. The load that will obtain the maximum power transfer is <br> (A) $1 \Omega$ resistance <br> (B) $1 \Omega$ resistance in parallel with 1 H inductance <br> (C) $1 \Omega$ resistance in series with 1 F capacitor <br> (D) $1 \Omega$ resistance in parallel with 1 F capacitor | (C) |
| 606 | 426 | A series RLC circuit has a resonance frequency of 1 khz and a quality factor $\mathrm{Q}=100$, If each of $\mathrm{R}, \mathrm{L}$ and C is doubled from its original value, the new Q of the circuit is <br> (A) 25 <br> (B) 50 <br> (C) 100 <br> (D) 200 | (B) |
| 606 | 427 | The short-circuit admittance matrix a two-port network is $\left[\begin{array}{cc}0 & -1 / 2 \\ 1 / 2 & 0\end{array}\right]$. The two-port network is <br> (A) non-reciprocal and passive <br> (B) non-reciprocal and active <br> (C) reciprocal and passive <br> (D) reciprocal and active | (B) |
| 606 | 428 | In IC technology, dry oxidation (using dry oxygen) as compared to wet oxidation (using steam or water vapor) produces <br> (A) superior quality oxide with a higher growth rate <br> (B) inferior quality oxide with a higher growth rate <br> (C) inferior quality oxide with a lower growth rate <br> (D) superior quality oxide with a lower growth rate | (D) |
| 606 | 429 | The source of a silicon $\left(n_{i}=10^{10}\right.$ per $\left.\mathrm{cm}^{3}\right) n$-channel MOS transistor has an area Of $1 \mathrm{sq} . \mathrm{mm}$ and a depth of $1 \mu \mathrm{~m}$. If the dopant density in the source is $10^{19} / \mathrm{cm}^{3}$, the number of holes in the source region with the above volume is approximately <br> (A) $10^{7}$ <br> (B) 100 | (D) |


|  |  | (C) 10 <br> (D) 0 |  |
| :---: | :---: | :---: | :---: |
| 606 | 430 | Drift current in the semiconductors depends upon <br> (A) only the electric field <br> (B) only the carrier concentration gradient <br> (C) both the electric field and the carrier concentration <br> (D) both the electric field and the carrier concentration gradient | (C) |
| 606 | 431 | A Zener diode, when used in voltage stabilization circuits, is biased in <br> (A) reverse bias region below the breakdown voltage <br> (B) reverse breakdown region <br> (C) forward bias region <br> (D) forward bias constant current mode | (B) |
| 606 | 432 | A silicon PN junction is forward biased with a constant current at room temperature. When the temperature is increased by $10 \geqslant \mathrm{C}$, the forward bias voltage across the PN junction <br> (A) increases by 60 mV <br> (B) decreases by 60 mV <br> (C) increases by 25 mV <br> (D) decreases by 25 mV | (D) |
| 606 | 433 | At room temperature, a possible value for the mobility of electrons in the inversion layer of a silicon $n$-channel MOSFET is <br> (A) $450 \mathrm{~cm}^{2} / \mathrm{V}-\mathrm{s}$ <br> (B) $1350 \mathrm{~cm}^{2} / \mathrm{V}-\mathrm{s}$ <br> (C) $1800 \mathrm{~cm}^{2} / \mathrm{V}-\mathrm{s}$ <br> (D) $3600 \mathrm{~cm}^{2} / \mathrm{V}-\mathrm{s}$ | (A) |
| 606 | 434 | Thin gate oxide in a CMOS process is preferably grown using <br> (A) wet oxidation <br> (B) dry oxidation <br> (C) epitaxial oxidation <br> (D) ion implantation | (B) |
| 606 | 435 | Compared to a p-n junction with $N A=N D=10^{14} / \mathrm{cm}^{3}$, which one of the following statements is TRUE for a p-n junction with $N A=N D=10^{20} / \mathrm{cm}^{3}$ ? <br> (A) Reverse breakdown voltage is lower and depletion capacitance is lower <br> (B) Reverse breakdown voltage is higher and depletion capacitance is lower <br> (C) Reverse breakdown voltage is lower and depletion capacitance is higher <br> (D) Reverse breakdown voltage is higher and depletion capacitance is higher | (C) |
| 606 | 436 | In an n-type silicon crystal at room temperature, which of the following can have a concentration of $4 \times 10^{19} / \mathrm{cm}^{-3}$ ? | (C) |


|  |  | (A) Silicon atoms <br> (B) Holes <br> (C) Dopant atoms <br> (D) Valence electrons |  |
| :---: | :---: | :---: | :---: |
| 606 | 437 | The ratio of the mobility to the diffusion coefficient in a semiconductor has the units <br> (A) $V-1$ <br> (B) $\mathrm{cm} \cdot V 1$ <br> (C) $V . \mathrm{cm}-1$ <br> (D) $V \cdot s$ | (A) |
| 606 | 438 | A silicon wafer has 100 nm of oxide on it and is furnace at a temperature above $1000^{\circ} \mathrm{C}$ for further oxidation. The oxidation rate <br> (A) is independent of current oxide thickness and temperature <br> (B) is independent of current oxide thickness but depends on temperature <br> (C) slows down as the oxide grows <br> (D) is zero as the existing oxide prevents further oxidation | (D) |
| 606 | 439 | The concentration of minority carriers in an extrinsic semiconductor under equilibrium is <br> (A) Directly proportional to doping concentration <br> (B) Inversely proportional to the doping concentration <br> (C) Directly proportional to the intrinsic concentration <br> (D) Inversely proportional to the intrinsic concentration | (A) |
| 606 | 440 | A heavily doped $n$-type semiconductor has the following data: <br> Hole-electron ratio $: 0.4$ <br> Doping concentration $: 4.2 \times 10^{8}$ atoms $/ \mathrm{m}^{3}$ <br> Intrinsic concentration $\quad: 1.5 \times 10^{4}$ atoms $/ \mathrm{m}^{3}$ <br> The ratio of conductance of the $n$-type semiconductor to that of the intrinsic semiconductor of same material and at same temperature is given by <br> (A) $5.0 \mathrm{E}-5$ <br> (B) 2000 <br> (C) 10000 <br> (D) 20000 | (D) |
| 606 | 441 | For a BJT, the common base current gain $\alpha=0.98$ and the collector base junction reverse bias saturation current $\mathrm{ICO}=0.6 \mu \mathrm{~A}$. This BJT is connected in the common emitter mode and operated in the active region with a base drive current IB $=20 \mu \mathrm{~A}$. The collector current IC for this mode of operation is <br> (A) 0.98 mA <br> (B) 0.99 mA <br> (C) 1.0 mA <br> (D) 1.01 mA | (D) |
| 606 | 442 | For small increase in $V G$ beyond 1V, which of the following gives the correct description of the region of | (D) |


|  |  | operation of each MOSFET <br> (A) Both the MOSFETs are in saturation region <br> (B) Both the MOSFETs are in triode region <br> (C) n-MOSFETs is in triode and $p$-MOSFET is in saturation region <br> (D) n - MOSFET is in saturation and $p$-MOSFET is in triode region |  |
| :---: | :---: | :---: | :---: |
| 606 | 443 | The input impedance $(Z i)$ and the output impedance $(Z 0)$ of an ideal transconductance voltage controlled current source amplifier are <br> (A) $Z i=0, Z 0=0$ <br> (B) $Z i=0, Z 0=\infty$ <br> (C) $Z i=\infty, Z 0=0$ <br> (D) $Z i=\infty, Z 0=\infty$ | (D) |
| 606 | 444 | An n-channel depletion MOSFET has following two points on its $I_{D}-V_{G s}$ curve: <br> (i) $V_{G S}=0$ at $I_{D}=12 \mathrm{~mA}$ and <br> (ii) $V_{G S}=-6$ Volts at $I_{D}=0 \mathrm{~mA}$ <br> Which of the following $Q$ point will given the highest trans conductance gain for small signals? <br> (A) $V_{G S}=-6 \mathrm{Volts}$ <br> (B) $V_{G S}=-3 \text { Volts }$ <br> (C) $V_{G S}=0 \mathrm{Volts}$ <br> (D) $V_{G S}=3 \text { Volts }$ | (C) |
| 606 | 445 | If $\beta D C$ is increased by $10 \%$, the collector-to-emitter voltage drop <br> (A) increases by less than or equal to $10 \%$ <br> (B) decreases by less than or equal to $10 \%$ <br> (C) increase by more than $10 \%$ <br> (D) decreases by more than $10 \%$ | (B) |
| 606 | 446 | In a full-wave rectifier using two ideal diodes, $V_{d c}$ and $V_{m}$ are the dc and peak values of the voltage respectively across a resistive load. If PIV is the peak inverse voltage of the diode, then the appropriate relationships for this rectifier are <br> (A) $V_{d c}=\frac{V_{m}}{\pi}, \mathrm{PIV}=2 V_{m}$ <br> (B) $I_{d c}=2 \frac{V_{m}}{\pi}, \mathrm{PIV}=2 V_{m}$ <br> (C) $V_{d c}=2 \frac{V_{m}}{\pi}, \mathrm{PIV}=V_{m}$ <br> (D) $V_{d c}=\frac{V_{m}}{\pi}, \mathrm{PIV}=V_{m}$ | (B) |
| 606 | 447 | An amplifier without feedback has a voltage gain of 50 , input resistance of $1 \mathrm{k} \Omega$ and output resistance of $2.5 \mathrm{k} \Omega$. The input resistance of the current-shunt negative feedback amplifier using the above amplifier with a feedback factor of 0.2 , is | (A) |


|  |  | (A) $\frac{1}{11} \mathrm{k} \Omega$ <br> (B) $\frac{1}{5} \mathrm{k} \Omega$ <br> (C) $5 \mathrm{k} \Omega$ <br> (D) $11 \mathrm{k} \Omega$ |  |
| :---: | :---: | :---: | :---: |
| 606 | 448 | Introducing a resistor in the emitter of a common amplifier stabilizes the dc operating point against variations in <br> (A) only the temperature <br> (B) only the $\beta$ of the transistor <br> (C) both temperature and $\beta$ <br> (D) none of the above | (C) |
| 606 | 449 | Crossover distortion behavior is characteristic of <br> (A) Class A output stage <br> (B) Class B output stage <br> (C) Class AB output stage <br> (D) Common-base output stage | (D) |
| 606 | 450 | In standing wave pattern on a transmission line <br> (A) voltage and current nodes coincide <br> (B) voltage nodes and current antinodes as well as current nodes and voltage antinodes coincide <br> (C) voltage and current antinode coincide <br> (D) both (A) and (C) | (D) |

